YUSHCHENKO, Yekaterina Logvinovna; MALINCVSKIY, Boris Nikolayevich; FOLISHCHUK, Galina Andreyevna; YADRENKO, Engelina Konstantinovna; NIKITIK, Andrey Ivanovich;

[The "Dnipro" control computer with a wide range of applications and its programming programme programmer's manual]
Upravliaiushchaia mashina shirokoga naznacheniia "Dnipro"
i programmiruiushchaia programma k nei; spravochnik rrogrammista. Kiev, Izd-vo "Natkova dumka," 1964. 279 p.

(MIRA 17:8)

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students in a wide var puters and programming	iety of specialties was are t	oking the course on com-
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KULINKOVICH, A.Ye.; TUSHCHENKO, Ye.L.

Basic algorithmic language. Kibernetika no.2:3-8 Mr-Ap '65.
(MIRA 18:5)

YUSHCHENKO, Ye.L. [IUshchenko, K.L.]

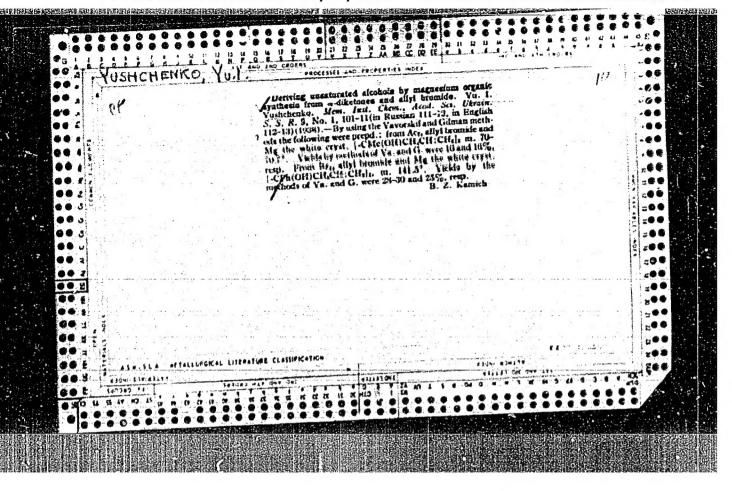
Automation of the process of composing programing programs. Dop. AN URSR no.6:715-717 '65. (MIRA 18:7)

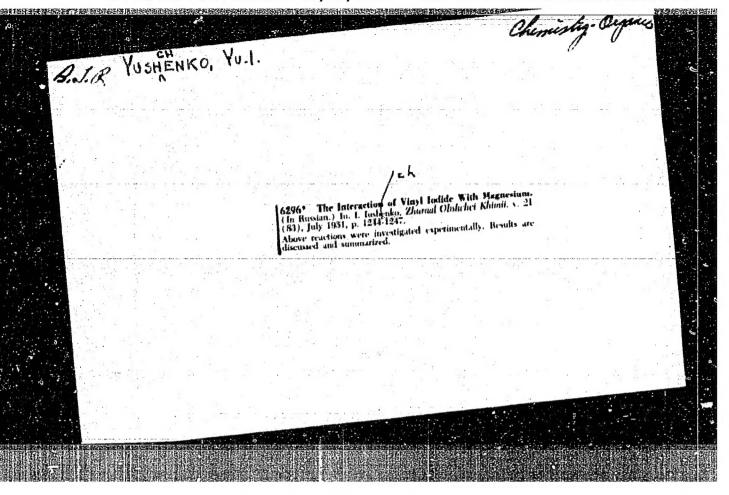
1. Institut kibernetiki AN UkrSSR.

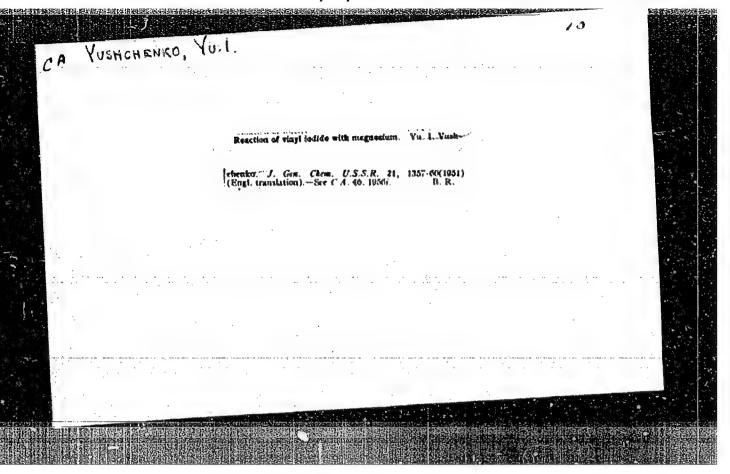
ACC NR: AM6016004 Monograph . Babenko, Lyudmila Petrovna; Dovgopolaya, Lyudmila Ivanova; Korniyenko, Galina Hikhaylovna; YUshchenko, YEkaterina Logvinovna Automatic programming system for the M-20 computer; translator from the address language. A manual (Sistema avtomaticheskogo programmirovaniya diya mashiny H-20; translyator s adresnogo yazyka. Spravochnoye rukovodstvo) Kiev, Naukova dumka, 1965. 153 p. 111us., biblio. (At head of title: Akademiya nauk Ukrainskoy SSR) 7750 copies printed. TOPIC TAGS: computer language, computer programming, algorithmic language, machine language PURPOSE AND COVERAGE: This book is intended for persons who use computers in their work or are engaged in the designing of automatic programming systems. The algorithmic address language used for describing computational, and information and logical processes, well as the respective programming program developed at the Institute of Gybernstics, AN UkrSSR for the Soviet H-20 computer, are described in detail. Hethods of programming a program and examples of programming are reviewed. The automated programming system developed by the authors makes it possible to increase the calculation rate on the K-20 computer by a factor of 10 to 15. Card 1/3

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YUSHCHENKOVA, N. I.

"Theory of the Steam Jet Vacuum Punp." Sand Phys-Lath Soi, Mathematics Inst Ensni V. A.
Stklov, Acad Sri USSk, 11 Feb 5h. Dissertation (Vechernyaya Moskva Moscow, 2 Feb 5h)

SO: SUN 196, 12 Aug 195h

Pi-ic

JUSACAEVKSTA, V L USSR/Physics - Vacuum pump

Pub. 153 - 19/24 Card 1/1

: Skobelkin, V. I., and Yushchenkova, N. I. Author

: Theory of the vapor-jet vacuum pump Title

: Zhur. tekh. fiz., 24, No 10, 1879-1891, Oct 1954 Periodical

: The authors investigate the interaction between the gas to be pumped Abstract

out and the supersonic vapor jet. They clarify the mechanism governing the process and thus are enabled to calculate the speed of pumping out of the gas and to determine the influence of the various parameters upon this speed. They note that their results differ from those obtained by

the USSR authors Lifshits and Rozentsveyg (ibid., No 8, 1952).

Institution : -

: April 3, 1953

Category : USSR/Atomic and Molecular Physics - Gases

D-7

Abs Jour : Ref Zhur - Fizika, No 1, 1957 No 932

Author

: Skobelkin, V.I., Yushchenkova, N.I. : Corrections to Article "Theory of Vapor-Jet Vacuum Pump." Title

Orig Pub : Zh. tekhn. fiziki, 1955, 25, No 2, 66

Abstract: Refers to Ref. Zhur. Fiz. 1955, 8952

Card : 1/1

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N.I. YUSHCHENKOVA, and KOSTERIN, S. I.

"Structure and Interaction of Supersonic Vapour Streams in Vacuum."

Report submitted for the Conference on Heat and Mass Transfer, Minsk, BSSR, June 1961.

KOSTERIN, S.I.; YUSHCHENKOVA, W.I.; BELOVA, N.T.; KAMAYEV, B.D.

Effect of rarefaction of a supersonic flow on the readings of impact-pressure probes. Inzh.-fiz.zhur. 5 no.12:16-22 D '62.

(HIRA 16:2)

1. Institut mekhaniki AN SSSR, Moskva.

(Aerodynamics, Supersonic)

YUSHCHENKOVA, N. I.; KOSTERIN, S. I.

"On the effect of kinetics of elementary reactions on ionization in stationary and non-stationary supersonic expansion and compression of gases."

report presented at the 10th Intl Combustion Symp, Cambridge, UK, 17-21 Aug 64.

Inst of Chemical Physics, AS USSR, Moscow.

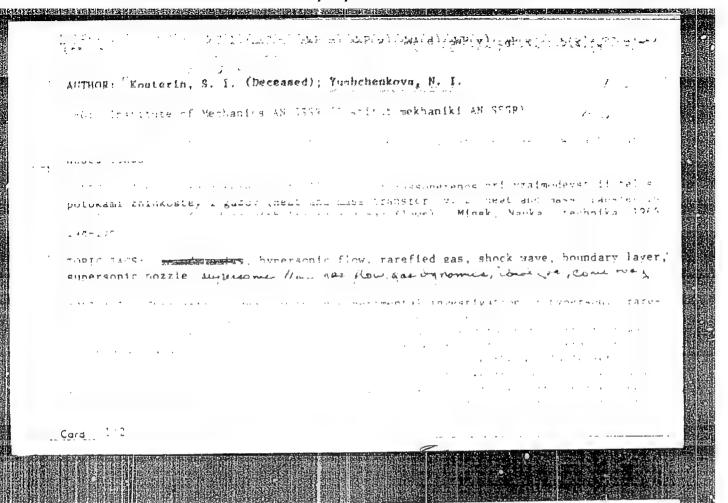
KOSTERIN, S.I.; YUSHCHENKOVA, N.I. (Moscow)

"Effect of kinetics on ionization at stationary and non-stationary supersonic extension and at instantaneous compression of a gas."

report presented at the 2nd All-Union Congress on Theoretical and Applied Mechanics, Moscow, 29 Jan - 5 Feb 64.

"On the effect of kinetics of elementary reactions in ionization in stationary and non-stationary supersonic expansion and compression of gases."														
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report submitted :	for 2nd All-U	nion Conf o	n Heat & Trans	sfer, Minsk, 4-1	.2 May
Mechanics Inst, A	S USSR.		· · · · · · · · · · · · · · · · · · ·		
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ACC NR. AP6036755

SOURCE CODE: UR/0020/66/171/001/0065/0068

AUTHOR: Zel'dovich, Ya. B. (Academicism); Kormer, S. B.; Krishkevich, G. V.; Yushchko, K. B.

ORG: none

TITLE: The problem of the smoothness of the detonation front in a liquid explosive

SOURCE: AN SSSR. Doklady, v. 171, no. 1, 1966, 65-68

TOPIC TAGS: shock wave, detonation front, detonation front profile, detonation front reflecting loss, liquid explosive

ABSTRACT: An analytical investigation of the light reflectivity of the detonation front in a liquid explosive (a mixture of nitric acid and dichloroethane) is presented, to explain the deviation of the experimental values of the reflection factor from the values calculated on the basis of the change of the refractive index in the wave front. The analysis uses earlier experimental data and yields a semi-quantitative description of the phenomenon as based on the wave theory of light reflection. The difference between the observed and calculated values of the reflection index, the analysis shows, can be ascribed to a certain degree of roughness on the detonation front comparable to the wavelength of the incident light. The degrees of roughness and the corresponding losses of reflected light intensities within the full range from purely specular to fully diffuse reflection were

Card 1/2

UDC: 532,5+535.0

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established. Conversely, the measured intensities of reflected light and dependence of the diffusely reflected portion on the angle of incidence characterize the degree and the average period of the roughness of the detonation front. The character of the roughness proved to be stationary under given conditions of detonation, while per turbations of higher orders leveled off very quickly. The deviation of the detonation front from a perfect specular surface is considered proven. The actual origin of the deviation, however, remains to be determined. At present, two explanations are considered possible: either it is a phenomenon resembling that observed earlier with gaseous detonation and only modified for the higher density of liquids; or it is initiated by inhomogeneities in the zone of chemical reaction, although no feedback—of these fluctuations on the process of reaction has been observed. The use of the laser beam as a light-source is being considered for a more detailed investigation of the profile of the detonation surface. Orig. art. has: 3 figures and 1 table.

SUB CODE: 20/ SUBH DATE: 18Ju166/ ORIG REF: 004/ ATD PRESS: 5107

Card 2/2

YUSHENAYTE, Ya.[Jusenaits, J.]; MEDONIS, A.R.; KAFLANAS, O., red.;
VISHOMIRSKIS, Ch.[Vyscarirekis, C.], tekhm. red.

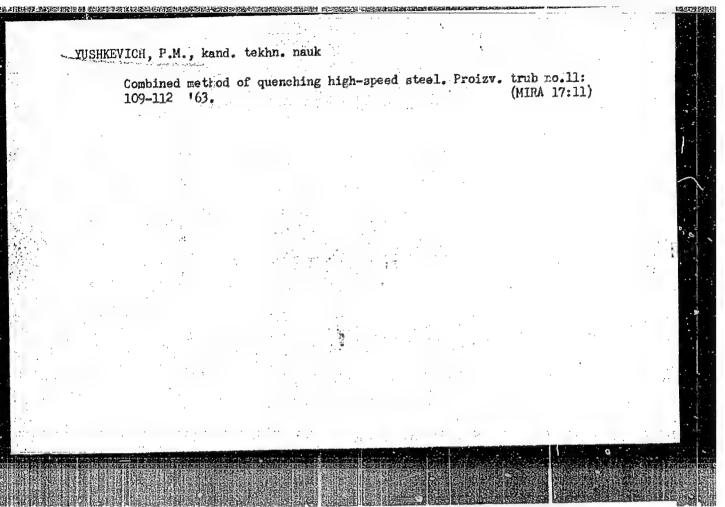
[The resort of Druskininkai]Kurort Druskininkai. 2. ispr.
i dop. izd. Viinius, Gos.izd-vo polit. i nauchn. lit-ry,
1962. 92 p.

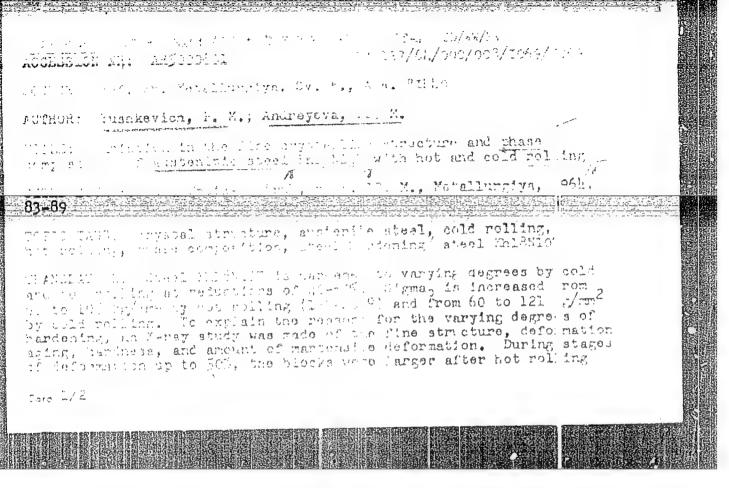
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(DRUSKININKAI--DESCRIPTION)

YUSHENAYTE, Ya. P., Cand Med Sci -- (diss) "Treatment of hypertensia" patients at Druskininkay Health Resort." Vil'nyus, 1958. 23 pp (Acad Sci Lithuanian SSR, Inst of experimental Medicine), 250 copies (KL, 35-58, 110)

-64-





5, 231 PAR

ACCESSION NR: AR5000601

20

than after cold rolling. With hot rolling to reductions more than 50%, the type II stresses are smaller than with cold rolling but the blocks are more broken up. Deformation aging was evaluated by a decrease in the gamma lattice period and was identical for both hot and cold rolling. With increase in the temperature of hot rolling the amount of martensite deformation formed decreases and becomes equal to zero at 2000 (point M_d). Thus the authors explain the fact that steel hardens more after cold rolling by the blocks breaking up, the increase in the density of the dislocations measured by X-ray, and the formation of martensite deformation. 3 figures, 11 liverature titles. Yu. Andreev.

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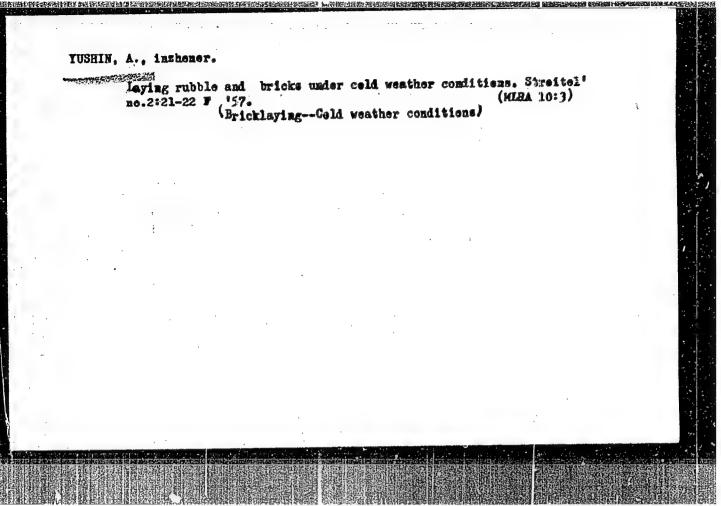
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Card 2/2

YUSHKEVICH, P.M., kand. tekhn. nauk; ANDREYEVA, Ye.M., inzh.

Change in the fine crystal structure and phase composition of Kh18N10T austenitic steel during hot and cold rolling. Proizv. trub no.12:83-89 164.

(MIRA 17:11)



APPROVED FOR RELEASE: 09/19/2001 CIA-RDP86-00513R001963230004-3"

Author: Iushin, A. A.

Title: Plasticity. (Plastichnost'.)

City: Moscow

YUSHIN, A. A.

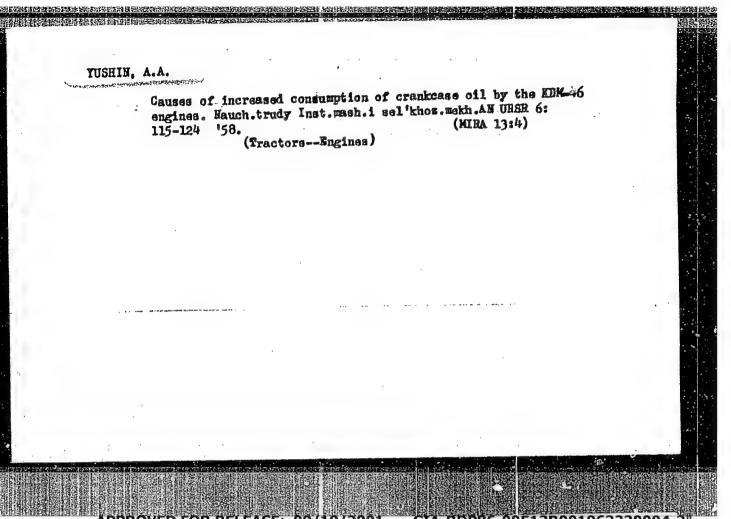
Publisher: State Printing House of Technical and Theoretical Edterature

Date: 1948

Available: Library of Congress

Source: Konthly List of Russian Accessions, Vol. L, Ro. 1, p. 19

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YUSHIN, A.A., kand tekhn nauk

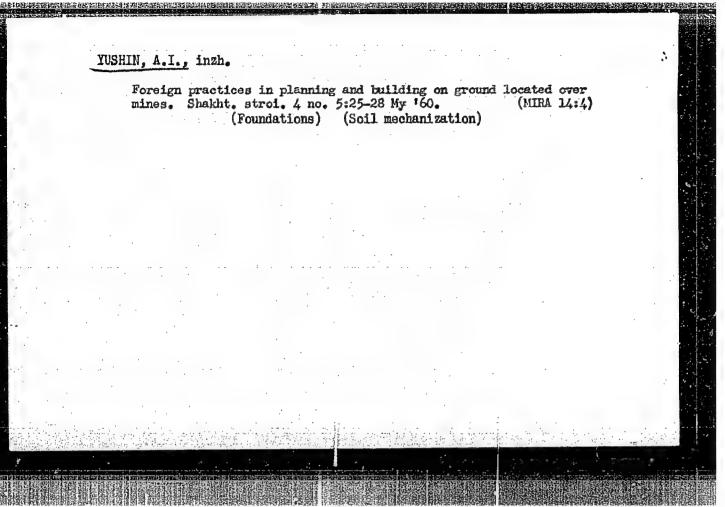
Study of the effect of special design features of the MTZ-52 tractor on its dynamic and operational indices. Trakt. i sel khozmash. 32 no.7: 4-6 Jl •62. (MIRA 15:7)

1. Ukrainskiy nauchno-issledovatel'skiy institut meklunizatsii i elektrifikatsii sel'skogo khonyaystva.
(Tractors)

HULLER, R.A.; YUSHIN, A.I.

"Temporary technical specifications on designing and building in areas being undermined." Reviewed by R.A.Kuller, A.I.IUshin. in areas being undermined. 158. (MIRA 11:11) Shakht.stroi. no.10:35-36 (Mining engineering) (Building)

APPROVED FOR RELEASE: 09/19/2001



APPROVED FOR RELEASE: 09/19/2001 CIA-RDP86-00513R001963230004-3"

MULLER, R.A., kand.tekhn.nauk; YUSHIN, A.I., inzh.; MELAMUT, L.Sh., inzh.

Temporary technical specifications for planning and constructing buildings and structures on ground located over mines. Shakht. stroi. 4 no. 5:29-30 My '60. (MIRA 14:4)

(Foundations) (Soil machanics)

USHIN, A.I.; VODOP'TANOV, V.N.; GITEL'MAN, M.V.; GRODZISKIY, L.I.

Designing a group of industrial buildings taking into account the deformation of foundations caused by underground workings.

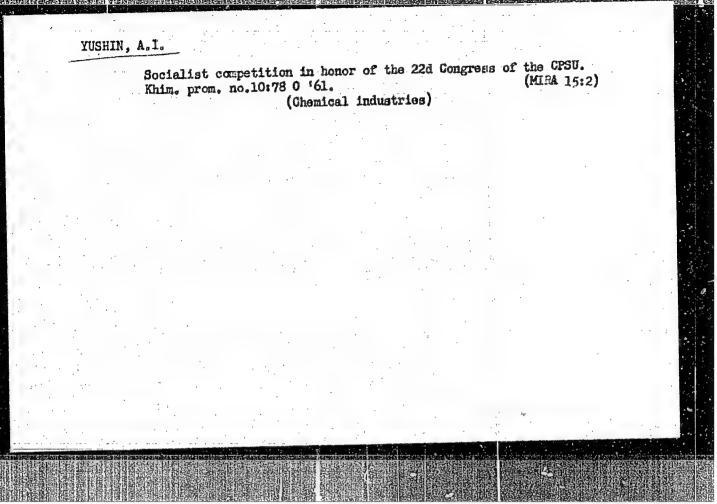
Prom. stroi. 38 no. 12:35-39 '60.

1. TSontrogiproshakin (for Jushin), 2. Enar'kovskoye otdeleniye Prometroyproyekt (for Godzinskiy).

(Foundations)

(Industrial buildings)

APPROVED FOR RELEASE: 09/19/2001 CIA-RDP86-00513R001963230004-3"



YUSHIN, A.I. (Moskva)

Design of residential and industrial buildings for uneven settling of the foundation. Stroi. mekh. i rasch. soor 4 no.1:40-44 '62. (MIRA 16:12)

KOLBENKOV, S.P.; MEDYANTSEV, A.N.; IOFIS, M.A.; KOROTKOV, M.V.;

MULLER, R.A.; YUSHIN, A.L.; MELAMUT, L.Sh.; KARGIN, G.P.;

GERTNER, P.F.; ZARETSKIY, K.S.; CHECHKOV, L.V., red.1zdva; MAKSIMOVA, V.V., tekhn. red.

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[Designing, constructing, and protecting buildings and structures on foundations undercut by mining] Proektirovanie, stroitel'stvo i okhrana zdanii i sooruzhenii na podrabatyvaemykh territoriiakh. Moskva, Gosgortekhindat, 1963. 451 p. (MIRA 16:8)

YUSHIN, A.I.; KOCHAROVA, I.K.

New pavilion entitled "Construction of Large-Panel Buildings under Complex Conditions." Osn., fund. i mekh. grun. 8 no.1:34-36 *66.

(MIRA 19:1)

TIMOFEYEV, S.V.; YUSHIN, A.I.; SHVEDOVA, S.N.

Study of the joint action of grillage and wall panels standing on the full-scale reinforced concrete units. Osn., fund. i mekh. grun. 7 no.5:18-21 '65. (MIRA 18:10)

STARITSYN, A.P., inzh., red.; MULLER, R.A., kand. tekhn. nauk, red.; YUSHIN, A.I., red.

[Instructions for designing buildings and structures on areas undercut by mining] Ukazaniia po proektirovaniiu zdanii i sooruzhenii na podrabatyvaemykh territoriiakh (SN 289-64). Izd. ofitsial'nos. Moskva, Stroiizdat, 1965. 81 p. (MIRA 18:6)

1. Russia (1923- U.S.S.R.) Gosudarstvennyy komitet po delam stroitelistva. 2. Gosstroy SSSR (for Staritsyn). 3. Vsesoyuznyy nauchno-issledovateliskiy institut gornoy geomekhaniki i marksheyderskogo dela (for Muller). 4. Nauchno-issledovateliskiy institut osnovaniy i podzemnykh sooruzheniy Gosstroya SSSR (for Yushin).

"APPROVED FOR RELEASE: 09/19/2001 CIA-RDP86-00513R001963230004-3 3/0016/04/038/004/0557/0962 Accession NR: AP4034582 AUTHOR: Devyaty*kh, G. G.; Yushin, A. S. TITIE: Equilibrium constants of the thermal dissociation reaction of simple volatile hydrides of the Group III-VI element hydrides. SOURCE: Zhurnal fizicheskoy khimii, v. 38, no. 4, 1964, 957-962 TOPIC TAGS: Group III hydride, Group IV hydride, Group V hydride, Group VI hydride, B sub 2 H sub 6, CH sub 4, SiH sub 4, GeH sub 4, PH sub 3, AsH sub 3, SbH sub 3, B sub 2 H sub 2 Se, H sub 2 Te, H sub 2, P sub 4, As sub 2, Sb sub 2, S sub 2, S sub 2, Te sub 3, thermal dissociation, volatile hydride, equilibrium constant, technologic deathermal retential heat affect isobaric isothermal potential, heat effect ABSTRACT: The aquilibrium constants for the thermal dissociation of the hydrides B2H6, CH4, SiH4, GeH4, PH3, AsH3, SbH3, H2S, H2Se, and H2Te as well as of the elements H2, P4, As2, Sb2, Se2, Te3 were calculated for the temperature interval of 300-1300K. Equilibrium constants of homogeneous gaseous reactions $\partial H_{1n} \rightleftharpoons \frac{1}{m} \partial_m + nH_3$

ACCESSION NR: AP4034582

were calculated by the statistical method from spectral characteristics of the molecules by the equation:

$$K_{\mathrm{p}_{\mathrm{g}}} = \frac{Q_{\mathrm{d}_{\mathrm{m}}}^{\prime / \mathrm{m}} Q_{\mathrm{H}_{\mathrm{c}}}}{Q_{\mathrm{d}_{\mathrm{d}_{\mathrm{m}}}} e^{-\Delta H_{\mathrm{e}_{\mathrm{g}}}^{*} / \mathrm{RT}}},$$

where Q_{2m} , Q_{H2} , $Q_{5\,H2n}$ are the statistical sum of elements as gas (5_m) , hydrogen and hydride, T is in K, ΔW_{1}^{\bullet} is the energy of dissociation of the hydride to the element and hydrogen. For reactions where the element separates as a solid:

equilibrium constants were calculated from:

$$R \ln K_{p_{11}} = \Delta \Phi^{\bullet} - \frac{\Delta H^{\bullet}_{\bullet 11}}{T}$$
where $\Delta \Phi^{\circ} = \Phi^{\circ}_{0 \circ \bullet} + n\Phi^{\circ}_{11} - \Phi_{01_{10}}$

Cord 2/3

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where $Q^* = -(Z^\circ - H^\circ_0)/T$, corrected isobaric-isothermal potential of the element or compound, $\Delta H^\circ_0 II$ is the heat effect at 0 K. All values are tabulated. The equilibrium constant values are graphically reviewed. All the hydrides except mothere, phosphine and hydrogen sulfide are completely broken down to the element and hydrogen in the given temperature range. Orig. art. has: 7 tables, 2 figures and 8 equations.

ASSOCIATION: Gor'kovskiy gosudaratvenny*y universitet im. N. I. Labachevskogo

(Gor'kov State Iniversity)

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ENCL:

greb63 SUEVITTED:

NO REF SOV:

OTHER: 018

SUB CODE:

SOV/124-58-10-11249

Translation from: Referativnyy zhurnal, Mekhanika, 1958, Nr 10, p 79 (USSR)

AUTHOR-

Yushin, A.Ya.

TITLE:

Experimental Investigation of the Local Heat Transfer of a Mixed Flow of Liquid in a Circular Tube (Eksperimental'noye issledovaniye mestnoy teplootdachi pri smeshannom dvizhenii zhidkosti v krugloy trube)

PERIODICAL: Sb. statey nauchn. stud. o-va Mosk. energ. in-ta, 1957, Nr 10, pp 164-177

ABSTRACT:

The paper is devoted to the investigation of the local heat transfer in the initial section of the tube when there are sections of laminar, transitional, and turbulent flows in the tube. Visual investigation on Reynolds apparatus of the transition phenomena of laminar flow into turbulent flow under isothermal conditions of liquid flow in the tube were conducted prior to undertaking experiments on the heat transfer. These observations showed that the transition-point position depends substantially on the value of RD and the conditions of entry into the tube, i.e., in a tube with a sharp-edged inlet the transition point starts much earlier than in a tube with a faired inlet.

Card 1/2

SOV/124-58-10-11249

Experimental Investigation of the Local Heat Transfer (cont.)

Heat-transfer investigation was conducted according to the B.S. Petukhov method of the thick-walled tube. The value of R_D varied from 3000 to 12,000 in the course of the experiments. Under conditions of smooth entry into the tube the distribution of local value of N_D along the length of the tube shows a clearly defined minimum corresponding to the incipience of the transitional region; its average position can be defined by the value of R_{crit} 52,000. This result coincides fully with the results of similar experiments carried out by Petukhov and Krasnoshchekov. Six experiments were conducted under conditions of a sharp-edged inlet into the tube the results of which are represented in the form of graphs. These experiments have shown that all other conditions being equal heat transfer depends substantially on the form of the inlet. Under conditions of a sharp-edged inlet the local values of N_D in the initial sector are considerably higher than under conditions of a faired inlet, although in the main section of the tube these values practically coincide. Bibliography: 4 references.

V.V. Kirillov

Card 2/2

8/096/60/000/010/013/022 11.4300 B194/B135 Yushin, A.Ya., Sukomel, A.S., and Petukhov, B.S., AUTHORS: Strigin, B.K. Experimental Investigation of the Heat Exchange during the Flow of Mercury in a Round Pipe in the TITLE: Laminar and Transitional Regions PERIODICAL: Teploenergetika, 1960, No 10, p 95 The investigation was carried out at low values of Reynolds number with a constant density of thermal flow through the walls. The experimental results are given in the form of generalised relationships covering the range of Reynolds numbers from 620 to 23,500 at P_{Θ} from 14 to 600. The experimental results are compared with those of other authors. ASSOCIATION: Moskovskiy energeticheskiy institut (Moscow Power Institute) Card 1/1

21,231

\$/143/61/000/007/002/004 DO53/D113

21,5240

Sukomel, A.S., Candidate of Technical Sciences, Docent; AUTHORS:

Yushin, A.Ya. and Strigin, B.K., Engineers

Investigation of the heat exchange during mercury flow in a TITLE:

round pipe at small Pecle numbers

Izvestiya vysshikh uchebnykh zavedeniy. PERIODICAL:

1961. 79-85

TEXT: Experimental results are given of the heat-exchange investigation during mercury flow in a round pipe at small Pecle numbers (Np). This investigation was carried out because little is known of the heat exchange during the flow of liquid metals in tubes, especially at small Np values.

The heat transfer was studied during the flow of mercury in laminar and transition regions under hydrodynamically and thermically stable conditions, and at a constant heat-flux density acting upon the pipe walls. The experimental setup (Fig. 1) consisted of (1) a round calibrated pipe made of soft carbon steel, 7.24 mm in internal diameter, 12.03 mm in external diameter, 1,504 mm long, and connected by rubber hoses with two mercury tanks; Card 1/64

24231

S/143/61/000/007/002/004 0053/0113

Investigation of the heat exchange ...

(2) an electric heater coaxially mounted with the 504 mm long working portion of the pipe (1); (3) a coaxial vacuum chamber; (4) four coaxial heat shields made from aluminum foil; (5) a thermostat; (6) a mercury mixer; auxiliary heaters (7 and 8); (9) a mercury cooler; (10) an electric motor for moving up and down the mercury tanks; and (11) a stroboscopic tachometer. The heat transfer was measured by 7 thermocouples afixed to the pipe (1). The heat-transfer coefficient was determined by the formula:

$$\alpha = \frac{q_1}{\pi d\Delta t}$$

where q_1 is the density of heat flux relative to the unit length of the pipe under test; d is the internal diameter of the pipe; and Δt is the calculated thermal head at the given cross-section. The heat-transfer measurements were conducted in the range from H_P 14 to 600, which corresponds to the range of Reynolds numbers from H_R 620 to 23,500 or to the Prandtl numbers: M_{Pr} 0.021 $\frac{1}{T}$ 0.026. The results obtained indicate that the heat transfer in Card 2/R4

24231 8/143/61/000/007/002/004 0053/0113

Investigation of the heat exchange...

the laminar region corresponds to the theoretical relationship

$$N_{Nu} = 4.36$$
; (1)

where N_{Nu} is the Nusselt number. The formula (1) is true for $N_{Re} \le 2,300$, which corresponds to $N_{P} \le 55$. The heat transfer in the transition region (Fig. 2) is described by the interpolated dependence

$$H_{Nu} = 4.36 + 0.0053H_{p}$$
. (2)

Deviations of the experimental N_{Nu} values from the formula (2) do not exceed 5%. This formula (2) is true for N_{Re} values from 2,300 to 23,500, which correspond to the N_P values from 55 to 600. The experimental data obtained for N_P > 400, or N_{Re} > 16,000 coincide with the formula N_{Nu} 5 + 0.014N_P 0.8, the error being + 5% (3).

Card 3/64

2\(\partial 2\)\(\frac{1}{3}\)\(\frac{1}{000}\)\(\frac{1}{007}\)\(\frac{1}{002}\)\(\frac{1}{004}\)\(\frac{1}{0053}\)\(\frac{1}{13}\)\(\frac{1}{000}\)\(\frac{1}

Investigation of the heat exchange...

This formula (3) describes the heat transfer of liquid metals during a turbulent flow (Ref. 5 and Ref. 6). It was derived by the Energeticheskiy institut AN SSSR (Power Engineering Institute of the AS USSR). There are 3 figures and 6 references: 4 Soviet-bloc and 2 English references. The references to the 2 English-language publications read as follows: B. Lubarsky and S.J. Kaufman, Report NACA No. 1270, Washington, 1956; E.A. Johnson, J.P. Hartnett, and W.J. Clabaugh, Trans. ASME, vol. 76, No. 4, p. 513, 1954.

ASSOCIATION: Moskovskiy ordena Lenina energeticheskiy institut (Moscow "Order of Lenin" Power Engineering Institute).

SUBMITTED: July 13, 1960

Card 4/69

APPROVED FOR RELEASE: 09/19/2001 CIA-RDP86-00513R001963230004-3"

/Lio 34

"APPROVED FOR RELEASE: 09/19/2001 CIA-RDP86-00513R001963230004-3 الاون s/020/61/136/006/01G/024 B104/B204 Petukhov, B. S. and Yushin. A. Ya. Heat exchange in the flow of a liquid metal in laminar 21, 4240 11.3950 Doklady Akademii nauk 3SSR, v. 136, no. 6, 1961, 1321-1324 AUTHORS: and intermediate regions TEXT: By means of the experimental arrangement shown in Fig. 1, the TEXT: By means of the experimental arrangement shown in Fig. 1, the heat exchange was studied on mercury with hydrodynamic and thermal stabilization of the flow puring filling marging was numified by TITLE: heat exchange was studied on mercury with hydrodynamic and thermal purified by During filling, mercury was purified by During filling, mercury was purified by ontainers were filled with argon from which distillation, and the two containers were filled with argon from the heat transfer coefficient was calculated or was necessary to be heat transfer coefficient was calculated or the heat transfer coefficient was distillation, and the two containers were filled with argon from which oxygen had been removed. The heat transfer coefficient was calculated to oxygen had been removed. The heat transfer density of the heat flow from the relation $\alpha = q_1/\pi d\Delta t$, where q_1 PERIODICAL: (kosl/m.hr) per unit length of the test tube; d is the inner diameter (kosl/m.hr) per unit length of the test tube; d is the inner diameter and tique to the tube; and the wall temperature, and the second to the tube; and the tube; are two the liquid temperature in a certain oross section. A correction of the the liquid temperature in a certain oross section. Which takes heat relation. from which t. is calculated. is discussed. the liquid temperature in a certain cross section. A correction of the relation, from which thin

Card 1/5

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s/020/61/136/006/010/024 B104/B204

CIA-RDP86-00513R001963230004

Card 2/5

transfer through the mercury and the tube in the longitudinal direction Heat exchange in the flow of a . into account. For the purpose of further reducing the effects produced into account. For the purpose of further reducing the effects produced by heat transfer in the longitudinal direction, the heat transfer to deficients were determined in cross sections which were at a distance coefficients were determined in cross sections which were at a distance of the heat of 19 d and 47 d from the beginning of the heated section of the tube. Thus, the numbers determined here are limits, i.e., they are minimum values. Tests with turbulent water showed satisfactory results. Values. Tests with turbulent water showed satisfactory results.

The experiments with mercury were carried out in the following ranges:

The from 14 to 600, Re from 620 to 23,500 (Pr = 0.021 + 0.026). In

Pe from 14 to 600, Re from 620 to 23,500 (Pr = 0.021 + 0.026).

The from 14 to 600, Re from 620 to 23,500 (Pr = 0.021 + 0.026).

The from 14 to 600, Re from 620 to 23,500 (Pr = 0.021 + 0.026).

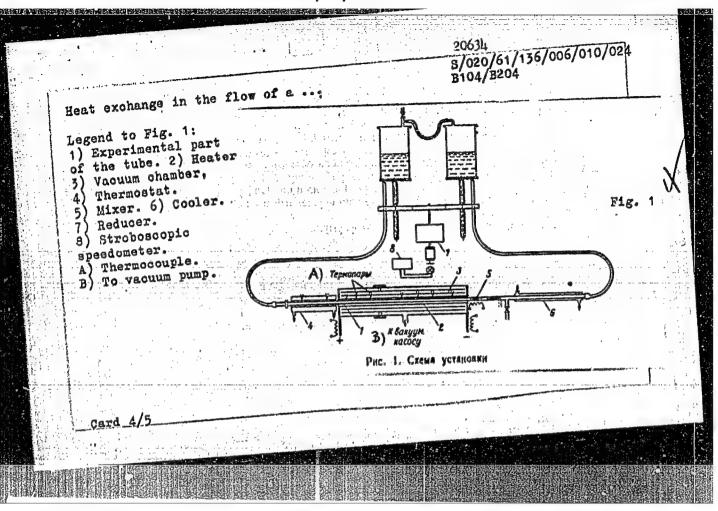
The from 14 to 600, Re from 620 to 23,500 (Pr = 0.021 + 0.026).

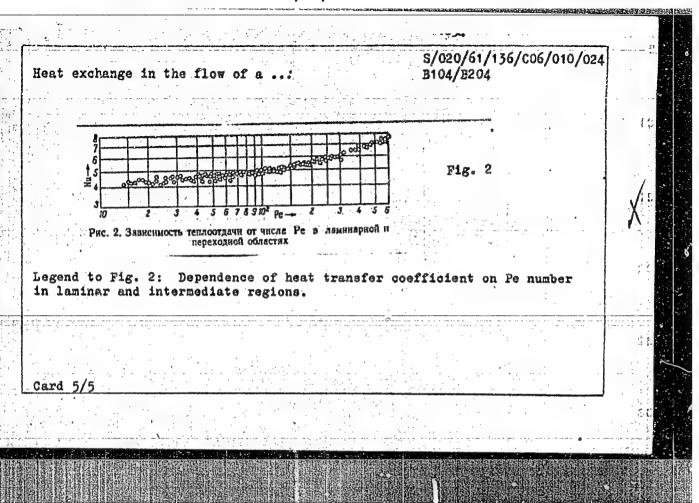
The from 14 to 600, Re from 620 to 23,500 (Pr = 0.021 + 0.026). Pe number. As may be seen, Nu = 4.36 for the laminar region, and Nu = re number. As may be seen, and a 4.70 for the laminar region, and and the 4.36 + 0.0053 Pe for the intermediate region. It is further noted that the results obtained here agree with an accuracy of ±5% with the formula Nu = 5 + 0.014 Pe with Pe 3 400 (Re = 1600) developed by the Energeticheskiy institut AN SSSR (Institute of Power Engineering of the AS USSR). It may further be seen that at the critical Reynolds number Re or = 2300 no considerable change of the dependence of the Nu number upon the Pe number occurs. Finally, the effect of cross grooves in the

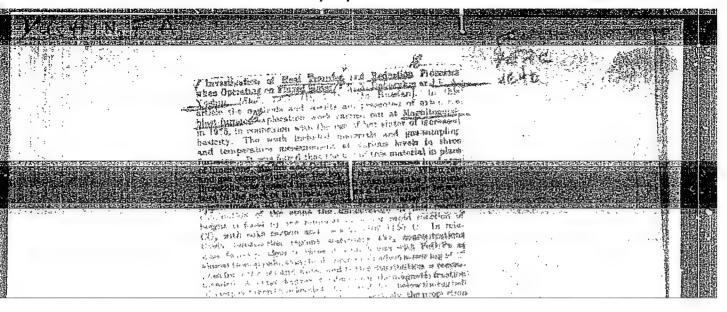
"APPROVED FOR RELEASE: 09/19/2001

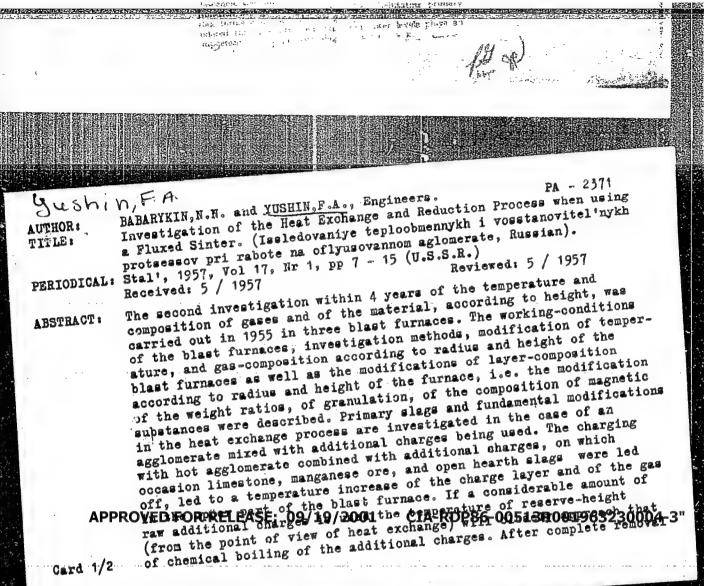
CIA-RDP86-00513R001963230004-3 5/020/61/136/006/010/024 B104/B204 tube upon the heat transfer is investigated. It is found that as a result Heat exchange in the flow of a of these cross grooves, considerable irregularities in the distribution of q over the experimental length of the tube occur, and that the use of cross grooves is not convenient at small Pe numbers, because this may cause considerable errors. M. V. Vol'kenshteyn, M. A. Yel'yashevich, B. I. Stepanov, L. S. Mayants, L. A. Ignat'yev, and I. K. Bayev are mentioned. There are 3 figures and 5 references: 3 Soviet-bloc and 2 non-Soviet-bloc. Moskovskiy energeticheskiy institut (Moscow Institute of Power Engineering) ASSOCIATION: September 14, 1960, by P. L. Kapitsa, Academician PRESENTED: August 24, 1960 SUBMITTED: card 3/5

CIA-RDP86-00513R001963230004









PA - 2371 Investigation of the Heat Exchange and Reduction Process when using a Fluxed Sinter.

of limestone it increases up to 1100 - 1150°. In those parts of the charge column, which are most charged, steady concentrations of CO2 were found to exist. Reduction velocity is here low, the highest being found in the upper and lower part of the column. During charging the ores divide mechanically into such with a great procentage of iron and into such with a small percentage of iron, a fact which facilitates the formation of primary slag, but reduces gas permeability to some extent. On the occasion of the formation of primary slags, those slags play an essential part which are conveyed from deeper horizons by the gas current.

ASSOCIATION: Metallurgic Combinate of Megnitogorsk PRESENTED BY:

SUBMITTED.

AVAILABLE: Library of Congress.

Card 2/2

AUTHOR: Babarykin, N.N., Engineer, and Yushin, F.A.

TITLE: Changes in the Blast Furnace Process when Operating with

Fluxed Sinter (Izmeneniya domennogo protsessa pri rabote na oflyusovannom aglomerate)

PERIODICAL: Stal', 1958, Nr 12, pp 1057-1065 (USSR)

ABSTRACT: An investigation of the blast furnace process during operation with fluxed sinter was carried out on three furnaces A, B and V in the Magnitogorsk Works and the results obtained compared with previous similar investigations. The working volumes of the furnaces:

A - 1180 m³, B and V - 1371 m³. The profiles of the furnaces and the position of levels at which sampling and measurements were carried out are given in Fig 1, and main operating data in Table 1. Sampling of the burden, the determination of temperature and composition of gas on the second and third levels were carried out on furnace B, a study of the composition of materials and gases along the bosh radius on furnace A, and of the composition and temperature of gases in the upper part of the stack and in the hearth on furnace V. Sampling

Card 1/5 of the stack and in the hearth on furnace V. Sampling of materials from the stack and the bosh was carried out

Changes in the Blast Furnace Process when Operating with Fluxed

with uncooled tubes of internal diameter 51 and 57 mm as was previously described (Ref 1). Materials from the tuyere zone were sampled with a special water cooled probe with a number of parallel cylindrical pockets (Fig 2). The temperature measurements in the stack were done with uncooled chromelalumel thermocouples. In the bosh and tuyere zone, thermocouples were cooled and on the lowest level molybdenum-tungsten thermocouples with quartz, graphite, molybdenum and berylium oxide sheaths were tested. The pressure, temperature and the composition of gas along the height of the burden column were determined as in Ref 1. Changes in the content of carbon dioxide (A) and temperature (B) along the furnace radius on I - IV levels are shown in Fig 3 (a - measurements in 1955, b - in 1956-57); the distribution of isotherms (A; °C) and lines of equal concentration of carbon dioxide (B; %) in the furnaces - Fig 4; changes in the static pressure along the height of the furnace -Table 2 and Fig 6 (a - 1956, b - 1957); the distribution of temperatures along the height of the furnace - Fig 5;

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 SOV/133-58-12-2/19

Changes in the Blast Furnace Process when Operating with Fluxed Sinter

chemical composition of burden materials on various furnace levels - Table 3; lines of equal mean degree of reduction - Fig 7 (results for 1956-57 A; for 1955 - B); mean chemical composition of metal beads collected from 3rd and 4th levels - Table 4; mean chemical composition of metal and slag from tuyere zone - Tables 5 and 6 respectively. It is concluded that: 1) the largest non-uniformity in the degree of reduction of iron oxides along the diameter was observed in the upper part of the This non-uniformity decreases as the burden descends towards lower levels. Mean degree of reduction of iron oxides for successive levels I-IV amounted to: % I - 22.6; II - 32.5; III - 57.6; IV - 85.7. An increase in the development of the reducing processes in the zone of moderate temperatures leads to a considerable improvement in the operating indices of a blast furnace. The analysis of changes in the content of sulphur on various levels supports the supposition that it circulates in the lower part of the burden column.

Card 3/5 The temperature range within which fluxed sinter attains

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SOV/133-58-12-2/19

Changes in the Blast Furnace Process when Operating with Fluxed

Sinter

a softened state decreases with increasing degree of reduction of iron oxides. In order to secure an even and stable furnace operation the zone of softening of the burden (which forms an additional resistance to the passage of gas) should be maintained on the level of the bosh or the bottom part of the stack. The formation of bosh or the bottom part of the Status and a steady sepadroplets of a liquid phase is preceded by a steady sepadroplet by a liquid phase is preceded by a steady sepadroplet by a liquid phase is preceded by a steady sepadroplet by a liquid phase is preceded by a steady sepadroplet by a liquid phase is preceded by a l ration of metal and slag inside lumps of sinter. good burden preparation the content of ferrous oxide in the primary slag is low and does not present any difficul-ties to an intensification of the rate of furnace driving. The presence of liquid slag in the mass of "dry" burden can be apparently explained by its being blown from lower furnace levels, as well as by considerable differences in the level of heat requirements of lumps of burden with an unequal degree of chemical proparation. The maximum gas temperature in the tuyere level (about 1990°C) was established to be at a distance of 0.4 m from the tuyere A partial transfer of sulphur from metal and nozzle.

Card 4/5

Changes in the Blast Furnace Process when Operating with Fluxed Sinter

slag into the gaseous phase takes place in the oxidising zone. The main mass of metal and slag flows down into the hearth through a peripheral zone the width of which does not exceed 2m from the furnace wall.

There are 7 figures, 6 tables and 4 references (all Soviet).

ASSOCIATION: Magnitogorskiy metallurgicheskiy kombinat (Magnitogorsk Metallurgical Combine)

Card 5/5

SOV/133-59-4-1/32

AUTHORS:

Babarykin, H.N., Agashin, A.A., and Yushin, F.A.,

Engineers

TITIE:

Determination of the Active Weight of Burden in an Operating Blast Furnace (Opredeleniye aktivnogo

vesa shikhty v deystvuyushchey domennoy pechi)

PERIODICAL: Stal', 1959, Nr 4, pp 289-291 (USSR)

ABSTRACT:

It is understood that the active weight of burden (kg/cm²) means the difference between the vertical pressure of the burden and the gas pressure supporting the burden: Qa = Qr - Pg. An analytical method of determining vertical pressure of the blast furnace burden based on Jansen's formula is proposed. Experimental determinations of the active weight of the burden at various furnace levels (down to 14.5m from the stock level) in an operating furnace were carried out. The measuring method was based on introducing a probe tube into the burden to a required level and measuring with a dynamometer (fig 1) the force required to retain the tube in the stationary state. The experimental set up is shown in Fig 2. The results of the determinations of static pressure of gas

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SOV/133-59-4-1/32

Determination of the Active Weight of Burden in an Operating Blast Furnace

and active weight of the burden as well as calculated values for vertical pressure of the layer of burden material at various furnace levels are assembled in the table. The experimental and calculated values for the vertical pressure of the burden within the limits of the "dry" zone agreed well (fig 3). The experimental data on changes in the degree of participation of the active weight in the vertical pressure of burden characterising the degree of driving of the blast furnace (the amount of passing gases) indicate that under conditions of a high top pressure operation the upper half of the furnace could be driven harder. This reserve of driving capacity of the upper part of the furnace can be utilised by blowing into the furnace

Card 2/3

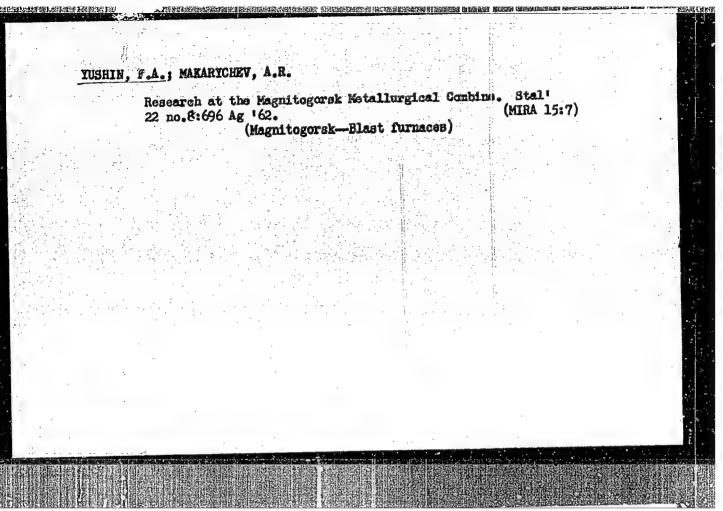
SOV/133-59-4-1/32

Determination of the Active Weight of Burden in an Operating Blast Furnace

stack some reducing gases. There are 3 figures, 1 table and 1 Soviet reference.

ASSOCIATION: Magnitogorskiy Metallurgicheskiy Kombinat (Magnitogorsk Metallurgical Combine)

Card 3/3



APPROVED FOR RELEASE: 09/19/2001 CIA-RDP86-00513R001963230004-3"

YUSHIN, F.A.; BAMARYKIN, N.H.

Studying the reduction processes in a blast furnace stark.

Stal' 24 no.11:968-975 N '64. (MIRA 18:1)

YUSHIN, F.A.

Intrustations in blast furnace downtakes. Stal' 25 no.2: 112-114 F'65. (MIRA 18:3)

1. Magnitogorakiy metallurgicheskiy kombinat.

。 日本的主理业场景域的图片,不在各两种的影響。

AGASHIN, A.A.; BABARYKIN, N.N.; VOLKOV, Yu.P.; GALATONOV, A.L.; KRYUKOV, N.M.; MALIKOV, K.V.; OSTROUKHOV, M.Ya.; PISHVANOV, V.L.; CHERNYATIN, A.N.; YUSHIN, P.A.

Experimental operation of blast furnaces on mazut and natural gas. Stal' 25 no.5:393-400 My '65. (MIRA 18:6)

1. Magnitogorskiy metallurgicheskiy kombinat; Vsesoyuznyy nauchnoissledovatel skiy institut metallurgicheskoy teplotekhniki i Chelyabinskiy nauchno-issledovatel skiy institut metallurgii.

KARIYEV, T.M., dotsent; VOLCKHVYANSKIY, A.M., kand. med. nauk; AEDURASHITOVA, M.V., kand. med. nauk; YUSHIN, G.I., kand. med. nauk

First Congress of Phtisiologists of Uzbekistan. Probl. tub. 41 no.5:89-92 '63. (MIRA 17:1)

YUSHIN, K.P., inzhener: AKOPYAN, G.M.

The SKH-4, new machine for harvesting underdeveloped cotton. Sel'khoznashina no.10:5-6 0'55. (MIRA 8:12)

1. Gosudarstvennoye spetsial'noye konstruktorskoye byuro po khlopku (Cotton-picking machinery)

YUSHIN, K.P., insh.

The SEO-4 cotton harvester for picking bypassed cotton. Trakt.i sel'khomash. no.8:32-33 Ag '62. (HRA 15:8)

1. Gosudarstvennoye spetsial'noye konstruktorskoye byuro khlopkouborochnykh mashin sovnarkhoza Uzbeksko; SSR. (Gotton-picking machinery)

107-57-2-50/56

AUTHOR: Yushin, N. (Aleksandrov)

TITLE: About the Performance of the "Rekord" TV Set. Experience Exchange (O rabote televizora "Rekord". Obmen opytom)

PERIODICAL: Radio, 1957, Nr 2, p 56 (USSR)

ABSTRACT: The town of Aleksandrov is situated 111 km northeast of Moscow.

Early commercial Soviet TV sets required additional equipment for reception in Aleksandrov. However, the "Rekord" TV set, fed by a 2-channel directional antenna, can function adequately without additional equipment. The antenna used by the author is described in "Radio", Nr 4, 1956.

There is I Soviet reference in the article.

AVAILABLE: Library of Congress

Card 1/1

YUSHIN, O.O., kandidat tekhnichnikh nauk; LYUSHIN, M.I., kandidat tekhnichnikh nauk.

Nork of C-80 and DT-54 tractors in surface tilling. Mekh. sil', hosp. 8 no.9:24-25 '57. (MIPA 10:9)

(Tractors) (Plowing)

TUSHIN, 0.0., kand, tekhn.nauk

Methode for investigating dynamic indices of wheeled tractors.

Mekh. sel'. hosp. 9 ne.9:28-30 S '58. (MIRA 11:10)

(Tractors)

VASIL'YEV, A.N., inzh.; GOROKHOV, N.G., inzh.; YUSHIN, P.V., inzh.

Production of 20KhGNR steel at the Kuznetsk Metallurgical Combine. Stal' 23 no.12:1085-1086 D '63. (MIRA 17:2)

1. Kuznetskiy metallurgicheskiy kombinat.

VCRCZHISHCHEV, V.I., inzh.; YUSHIN, P.V., inzh.; MASLOVA, V.N., inzh.

Effect of aluminum on the contamination by normetallic inclusions, the plasticity at high temperatures, and the mechanical properties of steel. Stal! 25 no.8:852-854 S 165. (MIRA 18:9)

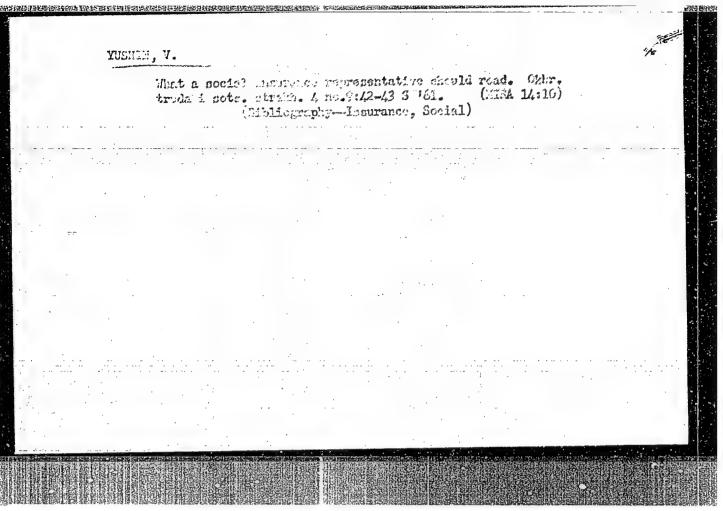
1. Kuznetskiy metallurgichoskiy kombinat.

ZHIL'TSOV, V.R.; ZELENOV, A.F.; KOKIN, A.G.; KOLOSOV, V.A.;
KOROBITSYN, M.D.; MALYAVIKSKIY, A.M.; NEFEDOV, Y.B.D.;
PAVLOV, A.V.; STEPANOV, T.A.A., prof.; SUVOROV, V.G.;
YUSHIN, S.I.; POCHTAREV, N.F., kand. tekhn. nauk, inzh.polkovnik, red.; KUZ'MIN, I.F., tekhn. red.

[Internal combustion engines; design and performance] Dvigateli vnutrennego sgoraniia; ustroistvo i rabota. [By] V.R.
Zhil'tsov i dr. Pod red. IU.A.Stepanova. Maskva, Voen. izd-vo
M-va obor. SSSR, 1955. 470 p.

(Internal combustion engines)

(Internal combustion engines)



APPROVED FOR RELEASE: 09/19/2001 CIA-RDP86-00513R001963230004-3"

DRIGHER, A. Ya.; YUSHE, V. G.

"Research in the Field of the Polymerization and orying of Gils and Storm of Fatty Acids," Part III.

"The Heat of Drying of Linesed Gil," Zhur. Obsheh.

Ehim., 10, No. 23-2h, 19h0. Laboratory of the Technology of Lecquers and Faints. Leningrad Chemico-Technological Institute. Received 26 November 1939.

Report U-1612, 3 Jan 1952

L 34071-66 EWT(d)/T IJP(c)

ACC NR. AP6013014

SOURCE CODE: UR/0410/66/000/001/0096/0100

AUTHOR: Yushin, V.I. (Novosibirsk)

9

ORG: none

TITLE: The influence of the spread of switch-on times on the determination of correlation functions of nonstationary processes [Paper presented at the 7th All-Union Conference on Automatic Control and Methods of Electrical Measurements held in Novosibirsk in September 1965]

SOURCE: Avtometriya, no. 1, 1966, 96-100

TOPIC TAGS: correlation function, correlation statistics, computer application, random process

ABSTRACTS: The evergrowing use of computers made the practical use of the results of the theory of nonstationary random functions possible. This, in turn, prompted the study of errors in the measurement of correlation functions of nonstationary processes which are of importance during the averaging over the set. The present note deals with one of the most specific errors of set correlation caused by the spread of the switch-on times and by the presence of stationary additive perturbation. The correlator is assumed to follow the algorithm

 $R_{xy}(t, \tau) = \frac{1}{N} \sum_{m=1}^{N} \left[x_i \left(t + \frac{\tau}{2} \right) - m_x \left(t + \frac{\tau}{2} \right) \right] \left[y_i \left(t - \frac{\tau}{2} \right) - m_y \left(t - \frac{\tau}{2} \right) \right], \tag{1}$

Card 1/2

UDC: 681.142.82

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nonstationar	y processes X	(t) and $Y(t)$; m _x (t) an	$am_{y}(t)$	respeci	ocese t -	m the reali matical ex the real the	me: and	
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L 03012-67 ENT(d)/T 1JP(c)

ACC NR: AP6028700

SOURCE CODE: UR/0410/66/000/003/0113/0121

AUTHOR: Yushin, V. I. (Novosibirsk)

28 B

ORG: none

TITLE: Optimum averaging intervals in the determination of statistical characteristics of a nonstationary process according to a single realization

SOURCE: Avtometriya, no. 3, 1966, 113-121

TOPIC TAGS: statistic analysis, correlation statistics, random process

ABSTRACT: In the determination of statistical characteristics of nonstationary random processes by averaging over the set of realizations, the large volume of computations required has led to the search for simpler procedures. The present author investigates the mean square errors of the determination of mathematical expectation and dispersion of a class of nonstation-ary random processes using the sliding averaging of a single trial. The results are in the form of expressions for optimum averaging intervals obtained using the minimum mean square error criteria. The knowledge of the mean correlation function of the process, of the mean correlation function of the square of the process, and of the correlation functions of the mathematical expectation and correlation are required. Rough estimates of all these functions can be made

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DERBIKOV, I.V.; AGUL'NIK, I.M.; BEN'KO, Ye.I.; YEKHANIN, Ye.V.; GRISHIN, M.P.; YUSHIN, V.I.

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Tectonics of the Mesozoic and Cenozoic mantle of the Western Siberian Lowland. Trudy SNIGGIMS no.11:63-155 '60. (MIRA 14:5) (Siberia, Western-Geology, Structural)

Stratigraphic position of horizons with iron deposits in Upper Cretateous and Paleogene sediments of the middle Ob' Valley.

Trudy SNIGGIMS no.6:150-162 '61. (MIRA 15:7) (Ob' Valley—Iron ores)

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SOURCE CODE: UR/0413/66/000/011/0102/0102

INVENTOR: Yushin, V. I.

ORG: None

TITLE: A digital correlator with magnetic drum memory. Class 42, No. 182414 [announced by the Institute of Automation and Electrometry, Siberian Department AN SSSR (Institut avtomatiki i elektrometrii Sibirskogo otdeleniya AN SSSR)]

SOURCE: Izobreteniya, promyshlennyye obraztsy, tovarnyye znaki, no. 11, 1966, 102

TOPIC TAGS: magnetic drum, computer component, digital system, flip flop circuit

ABSTRACT: This Author's Certificate introduces a digital correlator with magnetic drum memory. The installation contains an arithmetic unit which includes an adder—multiplier. Also included in the device are input and output units and a control unit. The correlator is designed for dealing with a large class of problems: operation as a matching filter, computation of the instantaneous correlation function and of the correlation function of nonstationary processes with averaging according to a set of realizations. In the control unit, the output of the device which forms the pulse for commencing readout is connected to the pulse inputs of the first and second switches whose potential inputs are connected respectively to the one and zero states of the first flip-flop. Connected to the set terminal of the first flip-

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flop are the input of the first potential polarity-reversing amplifier and the zero state of the second flip-flop (through a differential network). The output of the polarity-reversing amplifier is connected to the reset terminals of the first and third flip-flops and to the set terminals of the fourth and fifth flip-flops. The set terminal of the third flip-flop is connected through a differential network to the output of the first univibrator. The zero state of the fifth flip-flop is connected through a differential network to the input of this univibrator. The one state of the third flip-flop is connected to the potential input of the third switch. while the pulse input of this switch is connected to the output of the first switch. The output of the third switch is connected to the input of the second univibrator whose cutput is connected through a differential network to the reset terminal of the first-flip-flop. Connected to the reset terminal of the second flip-flop are the output of the second switch and the "initial state" bus. The set terminal of the second flip-flop is connected to the output of a revolution counter. The output of the circuit which shapes the synchro pulses for the cells is connected to the pulse outputs of the fourth and fifth switches whose potential inputs are connected respectively to the one and zero states of the sixth flip-flop. The output of the first polarity-reversing amplifier is connected to the reset terminal of the sixth flip-flop, while the output of the first switch is connected to the set terminal of this flip-flop. The output of the fourth switch is connected to the pulse input of the sixth switch, while the one state of the fourth flip-flop is connected to the potential input of the sixth switch. The output of the sixth switch is connected to

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the inputs of the seventh and eighth switches and that of the third univibrator. The output of this univibrator is connected through a differential network and an amplifier to the pulse inputs of the ninth and tenth switches. The output of the first switch is connected to the counting input of the fourth flip-flop. The one state of the fourth flip-flop is connected to the potential input of the sixth switch and to the inputs of the first, second and third coincidence circuits, and also through a differential network to the counting input of the fifth flip-flop. The reset terminal of the fifth flip-flop is connected to the potential inputs of the ninth and tenth switches and to the first inputs of the first and second coincidence circuits. The set terminal of the fifth flip-flop is connected to the potential inputs of the seventh and eighth switches and to the first input of the third coincidence circuit. The second input of the first coincidence circuit is connected to the zero state of the seventh flip-flop whose reset terminal is connected through a differential network to the zero state of the fifth flip-flop. The set terminal of the seventh flip-flop is connected to the output of the collector circuit in the operational control unit. Connected through the collector circuit to the reset terminal of the eighth flip-flop are the output of the device which forms the pulse for commencing readout and the output of the tenth switch. The output of the eighth switch is connected to the set terminal of the eighth flip-flop. Connected to the reset terminal of the ninth flip-flop are the output of the device which forms the pulse for commencing readout and the output of the seventh switch. The output of the ninth switch is connected to the set terminal of the ninth flip-flop. The one

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states of the eighth and ninth flip-flops are connected to the inputs of the first and second repeaters respectively. In the memory, the output of the first repeater is connected to the switch inputs of the readout emplifiers for the main shifting and nonshifting tracks. The output of the second repeater is connected to the switch input of the readout amplifier for the auxiliary track. The inputs of the readout emplifiers are connected to the readout windings of the corresponding heads. The output of each readout amplifier for the nonshifting track is connected to the set terminal of one of the four flip-flops for the nonshifting process. The outputs of the amplifiers for the shifting and auxiliary tracks are connected in pairs to four collector circuits whose outputs are connected to the set terminals of the corresponding flip-flops in the register for the shifting process. The outputs of the eighth and ninth switches are connected through the collector circuits to the bus for resetting the registers of the shifting and nonshifting processes. The one state of the fifth flip-flop is connected through a differential circuit, amplifier and relay contact which is closed in the "matched filter" state and open only during computation with cyclic shift to the circuit for resetting the register of the shifting process and to the pulse inputs of four switches whose potential inputs are connected to the data input, while their outputs are connected to the set terminals of the corresponding flip-flops in the register for the shifting process. Also incorporated in this unit is a shift cycle counter which has one input and two outputs. The input of the counter is connected through a differential network to the zero state of the fifth flip-flop. The zero state of the seventh flip-flop is connected through a dif-

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ferential network and an amplifier to the pulse input of the eleventh switch, while the zero state of the tenth flip-flop is connected through the same circuit to the pulse input of the twelfth switch. The outputs of the eleventh and twelfth switches are connected through the collector circuit to the set terminal of the seventh flip-The output of the eleventh switch is also connected to the reset terminal of the tenth flip-flop. The potential inputs of the eleventh and twelfth switches are connected to the one and zero states respectively of the tenth flip-flop. The output of the second potential polarity-reversing amplifier is connected to the set terminal of the tenth flip-flop and to the shift cycle counter reset. The input of this amplifier is connected to the zero state of the eleventh flip-flop. The "initial state" bus is connected to the reset terminal of the eleventh flip-flop, while a start pulse source is connected to its set terminal. The output of the second switch is connected to the pulse inputs of the thirteenth and fourteenth switches. while the output of the fifth switch is connected to the input of the fifteenth. The one state of the eleventh flip-flop is connected to the potential inputs of the thirteenth and fifteenth switches. The zero state of the twelfth flip-flop is connected to the potential input of the fourteenth switch. The reset terminal of the twelfth flip-flop is connected to the panel. The output of the fourteenth switch is connected through the collector circuit to the input of the third univibrator whose output is connected through a differential network to the set terminals of the eleventh and twelfth flip-flops. The second input of the collector circuit is connected to the output of an expectation circuit. The output of the thirteenth switch is

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connected to the reset terminal of the eleventh flip-flop, to the input of the revolution counter, and the ouput of the fifteenth switch is also connected through the collector circuit to the input of the cell counter. The output of the fifteenth switch is also connected through the collector circuit to the reset bus for the registers of the shifting and nonshifting processes. The output of the cell counter is connected through an amplifier two the pulse inputs of two groups of switches whose potential inputs are connected to the one states of the flip-flops in the registers of the shifting and nonshifting processes. The outputs of these two groups of switches are connected to the arithmetic unit. The output of the revolution counter is connected to the set terminal of the second flip-flop. The cell and revolution counters have an equal number of flip-flops.

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PETROV, P.S., dots.; BORISKIN, S.V., dots.; VASILENKO, N.A., starshiy prepod.; GERSHANOV, Ye.M., dots.; DEMENT'YEVA, A.N., starshiy prepod.; IL'IN, V.P., dots.; NIKITIN, D.P., starshiy prepod.; NIKITIN, D.P., starshiy prepod.; SHRANCHENKO, K.G., starshiy prepod.; YUSHIN, V.I., starshiy prepod.; POPOV, A.S., red.; MESHALKIN, V.I., tekhn. red.

[Book of the trade-union committee chairman; aid to the factory, plant and workshop committee chairman]Kniga predsedatelia komiteta profsoiuza; v pomoshch predsedateliu fabrichnogo, zavodskogo, tsekhovogo komiteta.
Moskva, Profizdat, 1962. 356 p. (MIRA 16:2)

1. Moscow. Vysshaya seochnaya shkola profdvizheniya. 2. Kafedra "Profsoyuznoye stroitel stvo" Moskovskoy vysshey zaochnoy shkoly prodvizheniya Vsesoyuznogo tsentral nogo soveta profsoyuzov (for all except Popov, Meshalkin). (Trade unions—Handbooks, manuals, etc.)

